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LEAK DETECTION WITH EXPANDABLE COATINGS

Final report on Contract NAS 8-26761 Control No. DCN 1-1-60-0010 (IF)

February 19 to December 18, 1971

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LEAK DETECTION WITH EXPANDABLE COATINGS

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February 19 to December 18, 1971

by

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Abstract

Objective of this study was to develop and evaluate a system for leak detection that could be easily applied over separable connectors and that would expand into a bubble or balloon if a leak were present. This objective was accomplished using thin films of Parafilm tape wrapped over connectors, which were then overcoated with a special formulation. The low yield strength and the high elongation of the envelope permit bubble formation if leakage occurs. This system may be appropriate for welds and other hardware besides separable connectors. The practical limit of this system appears to be for leaks exceeding 10^{-6} cc/sec. If this envelope is used to trap gases for mass spectrometer inspection, leaks in the range of 10^{-8} cc/sec. may be detectable.

FOREWORD

This report was prepared by Hauser Laboratories under contract NAS 8-26761 for the George C. Marshall Space Flight Center of the National Aeronautics and Space Administration. The work was administered under the technical direction of the Quality & Reliability Assurance Laboratory of the George C. Marshall Space Flight Center.

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I. INTRODUCTION

All missiles using liquid propellants have a large amount of piping using separable connectors. Each separable connector is a potential cause of leakage, and any leakage can be a serious malfunction. Rapid and sensitive detection of leaks at such connectors is thus a major concern for proper quality assurance and missile reliability.

Use of expandable coatings over separable connectors is a novel approach to the problem of leak detection, and this study was aimed toward developing materials appropriate for this purpose. The objective was to develop a system of coating/adhesive/release materials which could be tightly conformed over a separable connector and which would then form blisters or bubbles if the joint were to leak when pressurized. This blister or bubble should then be easily identified as a leakage point, and the material should be easily removable from the connector after tests have been completed.

II. CONCEPTS

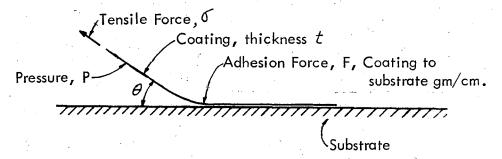
In many respects, the ideal material for this leak detecting coating would be a solid-phase soap bubble -- a material that could be painted on easily, and that would deform easily when pressurized. But unlike a soap bubble, the material would have long-term durability for tests that might last for at least several hours.

The mechanical properties of this ideal material would include low yield strength (in biaxial tension) and very high elongation (again biaxial tension) prior to rupture or pinhole formation.

Application properties of the ideal material would include opportunity for easy brushing over the connectors, rapid drying, and almost impossible flow characteristics -- smooth, uniform coverage over rough surfaces such as pipe threads and the ability to not flow into cracks and crevices.

Although a lifting and expanding balloon is hardly a "structure" some stress analysis has provided an understanding of the coating/hardware interface adhesion problems. This analysis relates to the yield strength of the film and its peel adhesion bond to the hardware.

The bubble lifting geometry can be simplified in two dimensions as:



Coating, thickness t Lift of bubble, L P, Pressure

Radius of bubble

Williams (1) describes the relations of bubble pressure, radius, and lift in relation to coating thickness and modulus of elasticity as follows:

$$r = \left(\frac{64 \text{ L E t}^3}{9 \text{ P}}\right)^{0.25}$$

2

Williams, M. L., "The Continuum Interpretation for Fracture and Adhesion."
J. Applied Polymer Science, vol. 13, 29–40, (1969).

The equation is applicable only for a very small amount of lift, and this condition truly exists if there is no transition in the adhesion of coating to substrate. Once pressure P has caused L to become finite, r has a finite value. The flatwise radius of the bubble can be maintained at a pressure less than the initial lifting pressure (since P is in the denominator of the above equation). In other words, the condition is unstable — if lift is initiated, r will continue increasing until the edge of the coating is reached, and then the bubble will leak at its edges.

This analysis underscores the importance of having a demarcation in the adhesion of coating to substrate -- a higher peel strength at the edges where seal is to be maintained than at the leak area where the bubble is expected to lift.

If the tensile force on the bubble (at any angle θ) exceeds the adhesion bond (at the same angle) of coating to substrate, the coating will lift slightly, leak at its edges and fail to indicate a leaking connector.

In order for the bubble to maintain its seal and grow by stretching, the yield strength of the bubble material must be low in relation to its adhesion peel strength to the substrate. This requirement is expressed mathematically as:

$$\int_{y}^{\infty} \langle F/t \rangle$$
 where $\int_{y}^{\infty} \langle F/t \rangle = \int_{y}^{\infty} \langle F/t \rangle$

F = adhesion to substrate gm/cm

t = coating thickness, cm

In order to obtain this demarcation in adhesive bond to the substrate, two combinations of materials can be used:

- a. A release material placed under the coating in the areas where ballooning is desired, and a coating with fair adhesion to the substrate.
- b. a coating with poor adhesion (easy release) to the substrate and a separate adhesive material applied at the interface where the bubble seal is desired.

Both concepts in materials combinations have been studied on this contract.

III. FORMULATIONS & APPLICATION PROPERTIES

Coatings, releases and adhesive materials were studied independently and then they were tested in combination for leakage performance tests. Major emphasis was given to the coatings.

A. Coating Materials

A large number of coating materials were considered, many were tried, and a few were tested. These studies started with some materials on the laboratory shelves and the scope was expanded as time and search indicated other prospects.

Thermoplastic elastomers and plasticized vinyl resins were the main emphasis in materials selection and formulation. The block copolymer of styrene and butadiene (Shell Kraton rubber) and thermoplastic urethanes were known to have high elongation and relatively high creep characteristics. Whereas the creep or viscous component of these polymers is often excessive

for mechanical applications, these elastomers were much too elastic by themselves and required a fair amount of modification with waxes and plasticizers.

An expanding bubble toy has intriguing characteristics pertinent to this study, and "Super Elastic Bubble Plastic" was given some consideration. Infrared spectral analysis revealed that this material was a vinyl acetate polymer. Whereas the material expands easily into an air-blown bubble, it quickly loses its solvent and forms a relatively hard, non-tacky bubble. Reformulation with permanent plasticizers rather than solvent might provide a practical expandable coating. Several vinyl formulations were prepared following recommendations of Union Carbide Corporation, Diamond-Shamrock Corporation and others.

Special additives were sometimes used to modify the surface tackiness, coating/substrate adhesion, flow characteristics or appearance. NP Antidust was used mostly as an anti-tack, and Zelec UN was used as an internal release additive to decrease the substrate adhesion of coatings.

A total of 136 formulations were outlined, as noted in Table 1, page 17. As each formulation was prepared, the application characterisitics were noted quantitatively and some adjustments were made immediately. Quick screening tests were frequently made to learn whether a good film was formed, and whether the coating had attractive properties of elongation and adhesion or release.

If the coating looked like a good prospect, its viscosity, tack time and dry time were measured. First viscosity tests were made with a Shell #2 viscosimeter, but most coatings were too viscous or dried (and plugged) too fast for this instrument. Shell #4 cup was used for most viscosity tests.

These application properties are noted in Table 1 along with the formulations. The number-coded suppliers of materials (except some common laboratory solvents and pigments) are noted in Table 2, page 39.

A number of parametric studies were made after good prospects had been identified. Four of these studies used Kraton elastomers with different amounts or types of wax or plasticizer additives. Figure 1, page 55 shows the effects of a polypropylene wax added to Kraton 1101. Figure 2, page 56 shows the very desirable attributes obtained by addition of Chlorowax 70 to Kraton 1101. Four plasticizers were then compared for the Kraton/Chlorowax 70 system in Figure 3, page 57. Finally the two alternative Kraton elastomers were compared with Kraton 1101 in Figure 4, page 58. All these studies used quantitative mechanical properties for comparison as follows:

Stress at 50% elongation
Permanent set after 50% elongation
Ultimate tensile strength
Ultimate elongation
Tear strength
90° peel adhesion strength

Details for these tests are discussed below in Paragraph IV-A.

A similar set of parametric studies was performed for the Bakelite VYHH vinyl resin with a variety of plasticizers and waxes. These data are shown in Figure 5, page 59.

Formula 105 was one of the best coatings of the study, and several variations were made therefrom. Dyes, Day-Glo pigments and solvents varied until Formula 130 was considered to provide the best combination of application and performance characteristics.

Subsequent formulations combining the coating in an aerosol with Propellant #12 indicated feasibility for spray application, but this alternative was not pursued to optimization.

B. Release Materials

Ten different tape and coating type releases were evaluated in this program, as outlined in Table 3, page 40.

The tapes were selected for ready conformability to the geometry of separable connectors. The self-vulcanizing silicone tape formed an excellent seal and release from the hardware, but coatings usually bonded to the silicone tape and reacted in an elastic manner because of the tape elasticity. The Teflon tape gave good release from both the hardware and the coating, but edges of this tape were too sharp and coatings were cut at these points.

None of the paint-on release materials was adequate. A greasy or nonwetting surface caused difficulties in the subsequent coating operation.

The best release material was Parafilm tape in 2-3 mil thickness. Parafilm is a waxy film that has high plastic elongation and a very low yield strength. When this material was used as a release tape, it could be stretched easily and then conformed tightly to the separable connector. Overcoats of the coating formulation bonded to the Parafilm, and the coating solvents helped to seal together the edges of the Parafilm. Parafilm and overcoating deformed together during pressurization, discussed below in Paragraph V-C.

The commercial Parafilm tape is produced in 5-mil thickness. Laboratory samples of 2-3 mil Parafilm were made by stretching the film about 100% between two sets of rollers. Delivery samples were made by the manufacturer, American Can Company, in a special production run.

C. Adhesive Materials

Seven adhesives were tried, as noted in Table 4, page 41. These adhesives were used only with coatings that had good release characteristics. Final formulations had adequate adhesion of coating to substrate and no adhesive was used in the final leak detection system.

The double tacky tape was ineffective when placed on hex nuts, due to lifting at the sharp bends. Otherwise each of the adhesives could be used with the appropriate type of coating (e.g. vinyl adhesive for vinyl coating and rubber adhesive for rubber coating).

IV. MECHANICAL PROPERTIES OF COATINGS

Pertinent tests were performed to evaluate in quantitative terms the mechanical properties of coatings. Test methods, results and selection criteria are discussed below.

A. Coating Selection Criteria

Tests were selected to identify those characteristics of the coatings that were most important in performance of leak detection objectives. Properties of low yield strength and high plastic elongation were considered to be essential. High tensile and tear strength would be helpful. Low or moderate peel adhesion strength would be needed, respectively, for a release coating or for an adherent coating. Tests and criteria are outlined below:

1. Tensile stress at 50% elongation.

Bubbles or blisters with 50% stretch of the film would be easily identified. A low stress at this elongation would signify low yield strength and easy distension of the bubble, preferably less than 30 Kg/sq.cm.

- 2. Permanent set after 50% elongation.
 - After the film has been stretched 50% and the load or pressure is decreased to zero, the film should not return in an elastic manner to original dimensions. A high permanent set would be desirable, preferably exceeding 50% of the stretch.
- 3. Ultimate tensile strength of the film may be of some significance, particularly in relation to toughness and durability during handling. A moderate ultimate tensile strength might provide a fair balance of durability and ease of removal. Strength between 1 and 30 Kg/sq.cm. was considered appropriate.
- 4. Ultimate elongation of the coating film was desired to be as high as possible, commensurate with other attributes. Elongation of 200% was considered to be the minimum acceptable.
- 5. Tear strength was desired to be a maximum, for best durability of the coating. This characteristic was considered secondary to the extensible properties noted above.
- 6. Peel adhesion was desired to be below 100 gm/cm for use as a release coating and above by t gm/cm if the coating was to be its own adhesive. As in Par. II above, by t is the product of the film yield strength and the film thickness.

B. Test Methods

The coating formulations were painted onto a release surface in order to obtain free films for testing. In most cases, polyethylene was used as the release surface, but with many of the Kraton/Chlorowax formulations no good adhesive surface was found. For these coatings, heavy paper was sized with animal glue prior to brush coats of the test formulation. Free films were then obtained by soaking the paper in water.

Tensile and tear test specimens were die-cut from these films. The tensile tests used specimens described in ASTM D412 and tests were performed at the rather slow crosshead speed 5 cm/minute (2 inches per minute). This permitted the operator to stop the test at the first 50% elongation, reverse the crosshead to learn

permanent set and then continue the test to learn ultimate strength and ultimate elongation. The force and crosshead position were recorded continuously during these tests.

Tear strength tests were performed according to ASTM D624, die C with crosshead a rate of 5 cm/minute (2 inches/minute). The maximum tear force was recorded, per unit of specimen thickness.

The peel adhesion specimens were made by coating a stainless steel coupon $2.5 \text{ cm} \times 15 \text{ cm}$ with two coats of the formulation. Then a cotton tape was placed onto one end of the coating and two more coats were applied. The tape was pulled at 90° angle to the stainless steel coupon at a rate of 5 cm/minute (2 inches/minute) and force was recorded continuously. Average peeling force per unit width was reported.

C. Results of Mechanical Tests

Coatings were tested with three replicate specimens and averages are reported in Table 5, page 45. Some of these data were discussed above in Figures 1-5.

As might be expected, this wide variety of coatings had properties that ranged from cheesy and sleazy to rough and tough. Some of the highly plasticized vinyl coatings would hardly support the weight of the dumb-bell shaped test specimen.

The properties of Formula #130, the recommended coating, are noted below:

Strength at 50% elongation Permanent set after 50% elongation Ultimate tensile strength Ultimate elongation Tear strength Peel strength 1.35 Kg/sq.cm 53% 1.61 Kg/sq.cm 860+% 1.66 Kg/sq.cm 47.4 gm/cm (peel after yielding) Parafilm is another component of the recommended leak detection system and its properties are:

Strength at 50% elongation 27.7 Kg/sq.cm.

Permanent set after 50% elongation 87%

Ultimate tensile strength 27.7 Kg/sq.cm.

Ultimate elongation 200%

Tear Strength 22.3 Kg/sq.cm.

V. PERFORMANCE TESTS

Tests were prepared to simulate the performance of the leak detection systems. These tests used separable connectors with the detection systems applied thereupon.

A. Performance Test Apparatus

Six sets of ten separable connectors were prepared using 1/2-inch stainless tubing with flare and flareless connectors. Each connection was mutilated with a groove by a triangular file so that it would leak. The ten connections were assembled with a quick disconnect fitting to provide rapid assembly for pressurization.

To evaluate the opportunity of handling different sizes of separable connectors, two additional "Christmas trees" were prepared using tubes of diameter 1/8 to 1" and a variety of step adapters. These also had a quick disconnect fitting for pressurization.

Air was used for pressurization of these test units, and a pressure regulator/gauge combination was used at the unit. This permitted gradual increase in pressure for each test.

Perfor

Performance tests were normally performed with the connectors under water, Figure 6, page 60. If air bubbles were observed without an obvious distension of the coating, the leak detector was faulty. If distension was observed, a pinhole or burst

failure would usually follow, and then bubbles would be observed. If neither distension nor air bubbles were noted, the coating system had closed off the leak. Sometimes this could be opened up at higher pressures (60 psi was the maximum pressure used), but if no leakage was obtained, the connector was considered to be "no test".

B. Application of Leak Detection Systems

First tests of the coatings were made by brushing or taping the appropriate release and/or adhesive and then by brushing on the extensible coating usually using two coats. The coating was allowed to dry overnight and then it was tested under water as noted above.

The number of distended bubbles or blisters and the number of leaking fittings were noted for each leak detection system. The lift distance was also noted for each bubble or blister.

As the detection systems developed, the combination of an extensible release tape and an extensible coating looked more and more attractive. The recommended system uses 3-mil Parafilm as a release tape and coating $^{\#}130$ as an overcoat.

The materials used for the recommended system consist of the following:

Parafilm tape, 3-mil thick by 1.5 cm wide by 8-10 cm long. Tape tightener -- a bundle of 10-15 elastic threads 20 cm. long, made of #600 Nylon elastic threads (Scoville Dritz)

Expandable coating, formula #130

Expandable coating, formula #130 Artists paint brush, #49 Fitch Fan Figure 7, page 61 illustrates the four steps for application of the leak detection system:

- A. A strip of Parafilm tape is pulled tightly against the tubing at one edge of the separable connector at least 2 mm beyond threads, insert or nut. The short end of the tape is pulled tightly against the tube and then it is folded toward the nut. The first wrap of the tape covers this short end.
- B. The tape is wrapped around nut and threads, pulled tightly into a helical pattern with at least 3 mm overlap for each turn. The tape is pulled tightly as it makes the transition between nut and thread diameter. Tape is terminated at a distance 3-4 mm beyond the last thread or insert. Termination is accomplished by stretching the Parafilm tape and breaking it at the tube.

The Parafilm tape wrap is now inspected to insure that a complete "mummy wrap" exists with no holidays.

C. Void volume within the Parafilm tape wrap must be minimized. To do this, the bundle of elastic threads is wrapped around the fitting at threads, inserts, bridges, or any place where the film is not in close contact with the hardware.

The tape wrap is again inspected to insure that complete, voidfree envelope.

D. A smooth brush coat of the coating #130 is applied over the Parafilm tape, extending 2-3 mm onto the tubing or fitting. After a 2-3 hour dry, a second brush coat of #130 is applied.

After the coating has dried 12-16 hours it should be inspected to insure that complete coverage has been obtained and to insure that the edges of the Parafilm tape have been sealed by the coating.

E. During or after system pressurization, the expanded bubble is inspected by both visual and tactile senses. If the bubble is not obvious, a finger can discern whether the film has lifted from the hex nut of the separable connector.

C. Results of Performance Tests

About 500 connectors were coated with various combinations of releases, adhesives and expandable coatings. Results of these tests are presented in Table 6, page 49.

In this table, the fraction of identifiable leaks (balloon bubbles) and the lift distance for these bubbles are the measures of performance.

Coating #130 with release #B10 provided the best and most consistent leak detection performance. Application of this system was described above. Bubbles were readily discerned in 105 of the 107 separable connectors where it was applied. Insufficient coverage of the coating #130 was cause for nondetection in the two tests, and insufficient inspection was cause for nondetection of the coverage. This was due to a violation of Quality Control Commandment #1 -- "The operator and the inspector shall be different persons responsible to different authorities."

Coating $^{\#}134$ was applied by aerosol over Parafilm tape, release B10, and it was effective in 7 of 9 connectors. This indicated the feasibility of aerosol application, but $^{\#}134$ was probably not an optimum formulation.

D. Reliability and Sensitivity of Leak Detection Systems

The recommended leak detection system described above appears to be highly reliable for large leaks when applied and inspected properly.

The smallest of the 107 leaks was measured to pass air at the rate of 2×10^{-4} cc/sec. (measured by water displacement). This leak was easily discernible with the expandable coating within a period of 1 hour.

Gas transmission rate of the Parafilm/#130 coating system was measured as 2670 cc/sq. meter 24 hr. atm. Since the coating over a hex nut of 0.5" diameter requires only 360 gm/sq.cm. or 5.1 psi pressure to cause yielding and ballooning,

the permeation pressure can not exceed this value. Thus the leak detection limit of this system is in the range of 7×10^{-7} cc/sec. The practical time limit of this system may be somewhere in the range of 10^{-6} cc/sec. over a period of 24 hour pressurization (0.1 cc. accumulation).

A further improvement is obvious in the area of application inspection. Since two coats of formula #A130 are used, the first coating would be better with an opaque white pigment and the second coating would be better with the Day-Glo pigment. This would provide an extra opportunity for inspecting the rather critical aspect of complete coverage by the coatings.

This leak detection system may be valuable in combination with mass spectrometer methods for extremely sensitive inspection. The envelope provided by this system could entrap the gases from a minute leak, and a hypodermic needle probe inserted into the envelope could identify the accumulation of this leakage. Such a system may be sensitive to 10^{-8} cc/sec. leak rate. Concern should be given to make sure that coating plasticizers do not interfere with the inspection system.

E. Removal of Leak Detection Systems

The unbonded portion of the leak detection wrapping is easily removed. A fingernail easily pierces the coating and the material pulls off cleanly. At the end where the coating is bonded onto the tubing, a rubbing action is needed to remove the formulation. Alternatively or additionally, a wipe with a solvent-moistened cloth quickly dissolves the residue. Toluene or trichloroethylene may be used as the solvent, depending upon concerns of flammability and vapor toxicity.

15

VI. CONCLUSIONS

Contract requirements have been met in the development and evaluation of an expandable coating system for leak detection. The system has not yet been evaluated in actual or simulated missile hardware to learn the practicality of application and the time/cost/reliability/sensitivity comparisons with alternative leak detection systems.

Coating #130 with 3-mil Parafilm tape provides an expandable coating system of leak detection that is sensitive to less than 10^{-6} cc/sec. leakage rate. It is readily visible and easily inspected for detection of leaks by visual and tactile senses. It is easily removable after use. In conjunction with a mass spectrometer, this system might provide 10^{-8} cc/sec. sensitivity.

Although the leak detection system was directed toward application on separable connectors, it may also have considerable utility for leak inspection of welds and other hardware. Slight modification of the tape/coating system could provide "band-aid" simplicity in application of leak detection patches.

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Table 1 - Formulas and Application Properties of Coatings

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A1	RTV 102 Silicone grease Freon TF Ethylene dichloride	20 10 35 6.4	15 11 13		Not Tested	
A2	Parafilm Zelec UN Freon TF Ethylene dichloride	30 0.5 35 235	1 <i>7</i> 13 13	too viscous (#2)	3+ hrs.	19+ hrs .
A3	R170857 Freon TF Ethylene dichloride	3 17.5 17.5	1 <i>4</i> 13		Not Tested Incompatible r	nixture
A4	Coverlac A-1114		22		Not Tested	
A5 ·	H P Latex				Not Tested	
A6	Spraylat SC-1073		22	•	Not Tested	
A7	Estane 5711 Vaseline Zelec UN Freon TF Acetone Ethylene dichloride	20 5 0.1 25 35 45	2 13 13		Not Tested	
A8	Kraton 1101 Zelec UN Freon TF Ethylene dichloride	20 0.2 65 65	21 13 13		Not Tested	
A9	Kraton 1101 Vaseline Zelec UN Freon TF Ethylene dichloride	20 5 0.2 70 70	21 13 13		Not Tested	

Table 1 - Formulas (Cont.)

1				•	•	
	•	!	Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A10	Hypalon 30 PPO #691-111 Modaflow Titania G 6099 Green Trichloroeth- ylene	50 6 0.25 60 6 218	13 15 18	too viscous (#2)	2.5	6.5
All	#11444 Tacki- wax Vaseline Zelec UN Freon TF Ethylene dichloride	20 5 0.2 45 45	5 13 13	too viscous (#2)	14.5	18+ hrs.
A12	Chlorowax 70 Freon TF Ethylene dichloride	20 30 40	10 13	too viscous (#2)	48	2.5+ hrs.
A13	Epolene X3259-11B Freon TF Ethylene dichloride	206565	12 13	·	Not Tested	
A 14	Epolene X3259-11C Freon TF Ethylene dichloride	20 40 40	12 13		Not Tested	
A15	Coverlac SC-271		22		Not Tested	
A16	Goodrich latex 60–457		2		Not Tested	
A17	RTV 102 Silicone grease Zelec UN Freon TF Ethylene dichloride	10 10 0.5 20 10	15 11 13 13	too viscous (#2)	90+	120+

Table 1 - Formulations (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A18	Spraylat SC=1073	20	22	too viscous	20	29
	Epon 828	2	21			
A19	Estane 5711 Vaseline	2 0 5	2	too viscous	3 ·	60
·	Zelec UN Paint Additive #7	0.1 0.05	13 11	(#2)		e e
	Freon TF Acetone Ethylene dichloride	25 35 45	13			
A20	Kraton 1101 Zelec UN Paint Additive #7	20 0.2 0.07	21 13 11	too viscous (#2)	13	33
	Freon TF Ethylene dichloride	65 65	13			
A21	Coverlac SC-271	20	22	•	Not Tested	
	Epon 828	2	21			
A22	Estane 5711 Epon 828 Freon TF Acetone Ethylene	20 4 24 35 45	2 21 13		Not Tested	
	dichloride					
A23	Kraton 1101 Epolene X3259-11C	20 10	21 12	too viscous (#2)	1	29
	Zelec UN Freon TF Ethylene dichloride	0.2 70 70	13 13	<i>\ - \</i>		

Table 1 - Formulations (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A24	Kraton 1101 Vaseline Zelec UN Paint Additive #7	20 10 0.2 0.14	21 13 11	too viscous (#2)	2	32
	Freon TF Ethylene dichloride	65 65	13	5	4 	
A25	Chlorowax 70 Trichloroeth- ylene	50 25	10	too viscous	56	.7+ hrs .
A26	Kraton 1101 Epolene X3259–11C Zelec UN Trichloroeth– ylene	10 5 0.1 100	21 12 13		Not Tested	
A27	Kraton 1101 Vaseline Zelec UN Paint Additive #7 Trichloroeth- ylene	10 5 0.1 0.07	21 13 11	too viscous (#2)	2	70+
A28	Estane 5711 Vaseline Zelec UN Paint Additive #7 Trichloroeth- ylene Acetone	10 2.5 0.05 0.025 35	2 13 11	·	Not Tested	
A29	Spraylat 1073 Day-Glo D13	20	22 9	too viscous	18	. 37
A30	Kraton 1101 Epolene Zelec UN Trichloroeth- ylene	10 7.5 0.1 75	21 12 13		Not Tested	

Table 1 - Formulations (Cont.)

		•				
			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A31	Kraton 1101 Chlorowax 70 Vaseline Zelec UN	10 5 5 0.1	21 10		Not Tested	
	Paint Additive #7 Trichloroeth- ylene	0.1 50	11			
A32	Estane 5711 Epolene X3259-11C Vaseline	10 5 5	2 12	too viscous	114	6.5+ hrs.
	Zelec UN Paint Additive #7	0.1 0.1	13 11			
	Acetone Trichloroeth- ylene	20 40				
A33	Spraylat SC-1073 Day-Glo D13	30 0.5	22 9	Not Tested	14	26
A34	Spraylat SC-1073 Day-Glo D13 Dioctyl phthala	60 1 te 4	22 9	too viscous (#2)	20	44
A35	Parafilm Toluene	15 85	17		Not Tested	
A36	Estane 5711 Vaseline Dioctyl phthala		2	too viscous (#2)	15	30
	Zelec UN Paint Additive #7	0.1 0.05	13 11			
	Freon TF Ethylene dichloride	25 45	13			

Table 1 - Formulations (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A37	Estane 5711 Vaseline Dioctyl phthalat Zelec UN Paint Additive	10 2.5 re 2 0.05 0.025	2 13 11	too viscous (#2)	34	66
	#7 Trichloroeth- ylene Acetone	35 17.5	11	,		
A38	Parafilm Day-Glo D13 Titania Toluene	15 1 5 85	17 9	too viscous (#2)	4+ hrs.	
A39.	Estane 5711 Vaseline Dioctyl phthala Methyl ethyl Ketone	20 5 te 2 60	2	too viscous (#2)	6	15
A40	Parafilm Kraton 1101 Day-Glo D13 Titania Toluene	10 5 1 5 85	17 21 9	too viscous (#2)	3.5+ hrs.	
A41	Spraylat SC-1073 Day-Glo D13 Dioctyl phthala	20 0.5 te 2	22 9	too viscous (#2)	10	31
A42	Coverlac SC271 Dioctyl phthala	20 te 2	22	too viscous	12	19
A43	Spraylat 1519A		22		Not Tested	
A44	Estane 5711 Vaseline Dioctyl phthala Methyl iso-Buty Ketone		2		Not Tested Incompatible i	mixture

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A45	Kraton 1101 Epolene X3259-11C Trichloroeth-	5 10 75	21 12	too viscous (#2)	7	41
	ylene			2	•.	
A46	Kraton 1101 Epolene X3259–11C	10 15	21 12		Not Tested	·*
	Trichloroeth- ylene	75				
A47	Kraton 1101 Chlorowax 70 Trichloroeth- ylene	10 10 70	21 10		Not Tested	
A48	Kraton 1101 Chlorowax 70 Trichloroeth- ylene	8 12 70	21 10	too viscous (#2)	8	20
A49	Bakelite VYHH Paraplex G-62 Chlorowax 70 Methy iso- Butyl Ketone Toluene	10 12.5 12.5 30	23 20 10	40 (#2)	24	44
A50	Kraton 3202 Chlorowax 70 Trichloroeth- ylene	8 12 70	21	25	12	26
A51	Kraton 3226 Chlorowax 70 Trichloroeth- ylene	8 12 70	21 10	109	7	31
A52	Kraton 3202 Zelec UN Vaseline Paint Additive #7 Trichloroeth-	10 0.1 5 0.07	21 13	too viscous (#2)	13	32
_	ylene				•	

Table 1 - Formulas (Cont.)

		,	Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A53	Kraton 3226 Zelec UN Vaseline Paint Additive #7 Trichloroeth-	10 0.1 5 0.07	21 13	too viscous (#2)	8	17
	ylene					
A 54	Kraton 1101 Epolene X3259-11C	10	21 12	too viscous (#2)	6	
	Zelec UN Trichloroeth- ylene	0.1 75	13			
	NP Antidust	1	19			
A55	Kraton 1101 Epolene X3259–11C	10 15	21		Not Tested	
	Zelec UN Trichloroeth- ylene NP Antidust	0.1 75	13			
A56	Kraton 1101 Chlorowax 70 Zelec UN Trichloroeth- ylene NP Antidust	10 10 0.1 70	21 10 13	too viscous (#2)	6	13
A57	Spraylat SC-1073 Dioctyl phthala	20	22	too viscous	29	54
A58	Spraylat SC-1073 Paraplex G-62	20	22	Not Tested	32	93
A59	Spraylat	20	22	Not	19	87
	SC-1073 Hercoflex 150	2	16	Tested		

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A60	Spraylat SC – 1073	20	22		Not Tested	,
	Resoflex R-296	2	4		4°	
A61	Spraylat SC – 1073	20	22	Not Tested	26	71
	Benzoflex 2-45	4	24			."
A62	Coverlac A1114 Dioctyl phthala	20	22		Not Tested	
A 63	Coverlac	20	22	too	15	29
A03	A1114	20	22	viscous	13	27
	Paraplex G-62	1	20			
A64	Coverlac A1114	20	22	Not Tested	10	46
	Hercoflex 150	1	16			
A65	Coverlac A1114	20	22		Not Tested	
	Resoflex R-296		4			
A66	Coverlac A1114	20	22		Not Tested	
	Benzoflex 2-45	1	24			
A67	Kraton 1101 Epolene X3259–11B	10	21	too	2	5
		10	12	viscous ([#] 2)		
	Zelec UN	0.1	13	,		
	NP Antidust Trichloroeth- ylene	105	19			
A68	Epolene X3259-11B	20	12		Not Tested	
	Zelec UN	0.1	13			
	NP Antidust Trichloro ethylene	100	19			

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A69	Spraylat 1073 Benzoflex 2–45	20 2	22 24	too viscous	13	38
A70	Kraton 3202 Chlorowax 70 Trichloroeth– ylene	10 10 70	21 10	167 ([#] 2)	7	22
A71	Kraton 3226 Chlorowax 70 Trichloroeth- ylene	10 10 70	21 10	too viscous (#2)	7	18
A72	Coverlac A1114 Paraplex G-62	20	22 20	Not Tested	8	20
A73	Coverlac A1114 Resoflex R-296	20	22 4	too viscous	8 .	29
A74	Coverlac A1114 Paraplex G-62	20 3	22 20	Not Tested	9	24
A75 .	Bakelite VYHH Paraplex G–62 Chlorowax 40 Methyl iso- butyl Ketone Toluene	10 12.5 12.5 30	23 20 10	75	Not Tested	
A76	Coverlac A2114		22		Not Tested	
A77	Kraton 1101 Chlorowax 70 Zelec UN NP Antidust Trichloroeth- ylene Carbon black	8 12 0.2 1 70	21 10 13 19		Not Tested	

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A78	Coverlac A2114 Carbon black	20	22		Not Tested	
A79	Carbon black Coverlac A2114 Paraplex G-62	2 20 1	22 20	5	Not Tested	
A80	Coverlac A2114 Resoflex R–296	20	22 4		Not Tested	
A81	Coverlac A2114 Dioctyl phthalat	20 e 1	22	349 ([#] 4)	Not Tested	
A82	Coverlac A2114 Benzoflex 2–45	20	22 24	too viscous	Not Tested	
A83	Kraton 1101 Chlorowax 70 Paraplex G-62 Trichloroeth- ylene	8 12 4 70	21 10 20	too viscous (#4)	Not Tested	
A84	Kraton 1101 Chlorowax 70 Paraplex G-62 Trichloroeth- ylene	8 12 8 70	21 10 20	too viscous (#4)	Not Tested	
A85	Kraton 1101 Chlorowax 70 Chlorowax 40 Trichloroeth- ylene	8 12 8 70	21 10 10	too viscous (#4)	Not Tested	

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A86	Kraton 1101 Chlorowax 70 Vaseline Trichloroeth- ylene	8 12 8 70	21 10		Not Tested	
A87	Kraton 1101 Chlorowax 70 Silicone grease Trichloroeth- ylene	8 12 8 70	21 10 11		Not Tested	
A88	Coverlac A2114 Paraplex G–62 Carbon black	20 2 2	22 20	too viscous (#4)	Not Tested	
A89	Coverlac A2114 Paraplex G–62 Carbon black	20 3 2	22	too viscous (#4)	Not Tested	
A90	Kraton 3202 Chlorowax 70 Zelec UN NP Antidust Trichloroeth- ylene Sudan Red	8 12 0.2 1 50	21 10 13 19	30 (#4)	Not Tested	
A91	Kraton 3226 Chlorowax 70 Zelec UN NP Antidust Trichloroeth- ylene Sudan red	8 12 0.2 1 50	21 10 13 19	28 (#4)	Not Tested	
A92	Kraton 1101 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- ylene	8 12 8 0.3 1 50	21 10 10 13 19	340 (#4)	Not Tested	
28	Sudan red	0.2	7	•		28

Table 1 - Formulas (Cont.)

					•	
			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A93	Kraton 1101 Kraton 3202 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- ylene	8 1 12 8 0.3 1 50	21 21 10 10 13 19	312 (#4)	Not Tested	
	Sudan red	0.2	7			
A94	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- ylene Sudan red	8 1 12 8 0.3 1 50	21 21 10 10 13 19	too viscous (#4)	Not Tested	
	,		•			
A95	Kraton 1101 Bakelite VYHH Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- ylene Sudan red	8 1 12 8 0.3 1 50	21 23 10 10 13 19	too viscous (#4)	Not Tested	
A96	Bakelite VYHH Paraplex G-62 Chlorowax 40 Chlorowax 70 Methyl iso- Butyl Ketone Toluene Sudan red	10 12.5 12.5 5 25 25	23 20 10 10	61 ([#] 4)	Not Tested	

Table 1 - Formulas (Cont.)

	•		Supplier	Viscosity sec o nds	Tack Time minutes	Dry Time minutes
A97	Bakelite VYHH Paraplex G-62 Chlorowax 40 Methyl iso- Butyl Ketone	10 15 15 25	23 20 10	50 (#4)	Not Tested	
	Toluene Sudan red	25 0.3	7			
A98	Bakelite VYHH Paraplex G-62 Chlorowax 40 Methyl iso-	10 12.5 12.5 25	23 20 10		Not Tested	,
	Butyl Ketone Toluene Parafilm Sudan red	25 25 5 0.3	17 7			•
A99	Bakelite VYHH Paraplex G-62 Chlorowax 40 Methyl iso- Butyl Ketone Toluene	10 12.5 12.5 25	23 20 10	too viscous (#4)	Not Tested	
	Epolene 3259-11C Sudan red	5	12 7			
A100	Bakelite VYHH Paraplex G-62 Chlorowax 40 Chlorowax 70 Methyl iso-	10 12.5 7.5 10 25	23 20 10 10	59 (#4)	Not Tested	
	Butyl Ketone Toluene Sudan red	25 0.2	7		· · ·	•
A101	Bakelite VYHH Paraplex G–62 Chlorowax 70 Methyl iso– Butyl Ketone	10 12.5 17.5 30	23 20 10		Not Tested	
	Toluene Sudan red	30 0.2	7			

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A102	Kraton 3202 Chorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- ylene Sudan red	8 12 8 0.2 1 50	21 10 10 13 19	33 (#4)	7	20
A103	Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- ylene Sudan red	8 12 8 0.2 1 50	21 10 10 13 19	23 (#4)	7	20
A104	Kraton 1101 Kraton 3202 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- ylene Sudan red	4 4 12 8 0.2 1 50	21 21 10 10 13 19	109 (#4)	7	20
A105	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- Sudan red	4 4 12 8 0.2 1 50 0.2	21 21 10 10 13 19	88 (#4)	7	20
A106	Kraton 3202 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- ylene Sudan red	8 12 8 0.4 1 50	21 10 10 13 19	50 (#4)	7	20

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A107	Kraton 3202 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- ylene Sudan red	8 12 8 0.6 1 50	21 10 10 13 19	149 (#4)	7	30
A108	Bakelite VYHH Kraton 3202 Chlorowax 70 Chlorowax 40 Paraplex G-62 Paint Additive #7 Zelec UN NP Antidust Methyl iso- Butyl Ketone Xylene Sudan red	10 5 20 5 12 0.1 0.3 1 30 40 0.3	23 21 10 10 20 11 13 19	too viscous (#4)	7	30
A109	Bakelite VYHH Kraton 3226 Chlorowax 70 Chlorowax 40 Paraplex G-62 Paint Additive #7 Zelec UN NP Antidust Methyl iso- Butyl Ketone Xylene Sudan red	10 5 20 5 12 0.1 0.3 1 30 40 0.3	23 21 10 10 20 11 13 19	50 (#4)	7	30

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A110	Kraton 3226 Chlorowax 70 Zelec UN NP Antidust Sudan red Trichloroeth- ylene	8 12 0.4 1 0.2 50	21 10 13 19 7	22 (#4)	3	5
A111	Parafilm Trichloroeth- ylene Water Barak	30 150 100 1	17	too viscous (#4)	Not Tested	
A112	Parafilm Trichloroeth- ylene	18 82	17	,	Not Tested	
A113	Parafilm Toluene	10 90	17	45 ([#] 4)	Not Tested	
A114	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN Trichloroeth- ylene Sudan red	6 2 8 8 0.4 40	21 21 10 10 13	345 (#4)	3	5
A115	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN Trichloroeth- ylene Sudan red	5 3 8 8 0.4 40	21 21 10 10 13	147 (#4)	3	15
	Juani Ioa	V • • •	•			

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A116	Kraton 1101 Bakelite VYHH Chlorowax 70 Chlorowax 40 Zelec UN Trichloroeth- ylene	6 4 8 12 0.4 50	21 23 10 10 13	.	Not Tested Incompatible n	nixture
	Sudan red	0.2	7			
A117	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN Trichloroeth- ylene	4 4 12 8 0.4 50	21 21 10 10 13	105 (#4)	5	15
	Sudan red	0.2	7			
A118	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- ylene Sudan red	4 4 12 8 0.2 0.5 50	21 21 10 10 13 19	78 (*4)	5	15
A119	Butyl TC-49 Trichloroeth- ylene	38 100	8			
A120	Kraton 3226 Butyl TC-49 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Day-Glo AX15-5 Trichloroeth- ylene	4 10 12 8 0.3 1 0.5	21 8 10 10 13 19		Not Tested Incompatible n	nixture

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time Dry Tin	
A121	Kraton 3226 Butyl TC-49 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust TiO 2 Trichloroeth- ylene	4 10 12 8 0.2 1 0.5	21 8 10 10 13 19	ç	Not Tested Incompatible mixture	•
A122	Kraton 3226 Butyl TC-49 Paraplex G-62 TiO ₂ Trichloroeth-	4 5 20 0.5	21 8 20		Not Tested Incompatible mixture	
A123	ylene Kraton 3226 Butyl TC-49 Actinol EPG	4 5 3 0.5	21 8 1		Not Tested Incompatible mixture	
	TiO ₂ Trichloroeth- ylene	40				
A124	Kraton 3226 Butyl TC–49 Titania Trichloroeth– ylene	4 5 0.5 40	21 8		Not Tested Incompatible mixture	
	Benzoflex	3	24			
A125	Kraton 3226 Butyl TC–49 Titania Trichloroeth– ylene	4 5 0.5 40	21 8		Not Tested Incompatible mixture	
	Hercoflex	3	16			

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A126	Kraton 3226 Butyl TC-49 Titania Trichloroeth- ylene	4 5 0.5 40	21 8	5	Not Tested Incompatible	mixture
	Resoflex	4	4		·	.* .
A127	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Day-Glo AX15-5 Toluene	4 4 12 8 0.2 1 0.5	21 21 10 10 13 19 9		Not Tested	
A128	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Day-Glo AX15-5 Toluene	4 4 12 8 0.2 1 0.5	21 21 10 10 13 19 9		Not Tested	
A129	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Titania Trichloroeth- ylene	4 4 12 8 0.2 1 0.5 50	21 21 10 10 13 19		Not Tested	

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A130	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Titania Day-Glo AX15-5 Toluene	4 4 12 8 0.2 1 0.5 0.5	21 21 10 10 13 19	92	5	210
A131	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- ylene Sudan red Freon 12	4 4 12 8 0.2 1 50 0.2 81.3	21 21 10 10 13 19		Not Tested	
A132	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Trichloroeth- ylene Sudan red Freon 12	4 4 12 8 0.2 1 80 0.2 90.6	21 21 10 10 13 19		Not Tested	
A133	Kraton 1101 Kraton 3226 Chlorowax 70 Chlorowax 40 Zelec UN NP Antidust Titania Day-Glo AX15-5 Toluene Freon 12	4 4 12 8 0.2 1 0.5 0.5	21 21 10 10 13 19 9		Not Tested	

Table 1 - Formulas (Cont.)

			Supplier	Viscosity seconds	Tack Time minutes	Dry Time minutes
A134	Kraton 1101	4	21		Not Tested	
	Kraton 32 2 6	4	21			
	Chlorowax 70	12	10		·	
	Chlorowax 40	8	10		v	
•	Zelec UN	0.2	13	•		
	NP Antidust	1	19			.*
	Trichloroeth- ylene	75			·	
	Sudan red	0.2	7		•	
•	Freon 12	62	13			
A135	Kraton 1101	4	21		Not Tested	
	Kraton 3226	4	21			
,	Chlorowax 70	12	10			
•	Chlorowax 40	8	10	7 .		
	Zelec UN	0.2	13			
•	NP Antidust	1	19			
*	Titania	0.5				
	Day-Glo AX15-5	0.5	9			
	Toluene	45				
	Freon 12	38	13			
	Modaflow	2	18			
A136	Kraton 1101	4	21		Not Tested	
i	Kraton 3226	4	21			
	Chlorowax 70	12	10			
	Chlorowax 40	8	10		•	
	Zelec UN	0.2	13			
	NP Antidust	1	19			
	Trichloroeth- ylene	75				
•	Sudan red	0.2	7			

Table 2 - Sources of Materials Used in Formulations

No.	Supplier
1	Arizona Chemical Company
2	B. F. Goodrich
3	Cabot Corporation, Oxides Division
4	Cambridge Industries Company
5	Central Scientific Company
6	Chas. Pfizer & Company, Inc., Williams Division
7	Chemical Sales Corporation
8	Chemical Sealing Corporation
9	Day-Glo Color Corporation
10	Diamond Shamrock Corporation
11	Dow Chemical Company
12	Eastman Chemical Products, Inc.
13	E. I. DuPont de Nemours & Company, Inc.
14	Firestone Synthetic Rubber & Latex Company
15	General Electric Company, Silicone Products Division
16	Hercules Powder Company
17	Marathon Products
18	Monsanto Company
19	National Polychemicals, Inc.
20	Rohm & Haas
21	Shell Chemical Company
22	Spraylat Corporation
23	Union Carbide Corporation, Chemicals & Plastics
24	Velsicol Chemical Corporation

Table 3 - Release Materials

No.	Material	Source
B-1	Silicone self-vulcanizing tape 5-mil thick, 0.5 inch wide.	Permacil #P2650
B-2	Teflon tape. Ribbon dope thread sealant, 0.35 milby 0.5 inch wide.	Permacel #P-412
B-3	Teflon telomer aerosol spray.	Ram #GS-3
B-4	Teflon telomer dispersion.	duPont Vydax AR
B-5	Kel-F grease, 37% in trichloroethylene.	3M Company
B-6	Silicone stopcock grease.	Dow-Corning Corporation
B-7	Reso-Part solution of polyvinyl alcohol	Plasticrafts, Inc. Denver, Colorado
B-8	Silicone rubber, RTV-E 50% solution in toluene with curing agent E	Dow-Corning Corporation
B-9	Parafilm, 5-mil, cut into tapes 1.5 cm wide	American Can Company Neenah, Wisconsin
B-10	Special Parafilm, 2-3 mil thick, cut into tapes 1.5 cm wide	American Can Company

Table 4 - Adhesive Materials

No.	Material	Source
C-1	Rubber adhesive Scotch-Grip 847	3M Company
C-2	Rubber adhesive Scotch-Grip 4693	3M Company
C-3 _.	Vinyl adhesive Scotch-Grip 2262	³ 3M Company
C-4	Rubber adhesive Pliobond	Goodyear trademark, local hardware sales
C-5	Vinyl adhesive Penncraft Household Cement	J.C. Penney Co.
C-6	Double-tacky tape Scotch #665	3M Company
C-7	Pressure-sensitive latex adhesive Maniflex #1608	Manufacturers Chemical Co.

Table 5 - Mechanical Properties of Coatings

	Stress @ 50% Strain 2 kg/cm	% Set at 50% Elong- gation	Ultimate Tensile Strength kg/cm ²	Total Elongation %	Tear Strength	90° Peel Strength
A18	5.4	29.4	33.4	2 30	9.3	51.8
A19	29.2	60.6	77.4	560	50.7	
A20	4.89	13.6	21.3	750	8.75	5.54
A21	4.79	48.9	22.8	200	6.91	64.3
A24	7.28	15.6	36.1	810	13.2	7.3
A26	12.0	18.6	59.6	740	16.7	178
A27	7.45	9.9	53.2	890	17.2	33.9
A28	45.0	57 . 2	104.0	490	53.1	1.79
A31	4.47	14	30.3	848		69.5
A33	25.8	71.0	79.5	140	20.6	13.7
A41	4.57	26.9	27.3	230	7.14	12.7
A42		Material was	too sticky to p	repare samples fr	om	21.1
A43			To sticky fo	or samples		19.2
A45	7.52	31.5	18.1	630	8.69	110.7
A46		,	Too sticky		-	86.9
A47			Too sticky			526.7
A48	28.1	37.0	125.0	710	44.9	
A49	9.58	23	1.75	163		
A50	29.8	84	37.5	240	27.0	357+
A51	29.0	78	35.9	430	28.1	357+
A52	1.46	To small to measure	8.2	630	3.29	5.3
A53	1.04	Too small to measure	7.69	690	3.16	5.4

Table 5 - Mechanical Properties.

				•		
	Stress @ 50% Strain 2 kg/cm	% Set at 50% Elong– gation	Ultimate Tensile Strength kg/cm ²	Total Elongation %	Tear Strength	90° Peel Strength
A54	7.81	24.7	41.9	730	9.6	5.65
A55	4.96	28.5	13.4	600	6.65	9.76
A56	38.7	24.7	184.0	820	36.9	4.16
A57	3.57	31.2	73.0	310	6.52	12.4
A58	3.2	21.7	56.2	230	9.56	18.3
A59	3.26	25.4	51.5	300	7.78	13.9
A60	2.11	34.5	3.46	100	2.94	16.7
A61	2.8	22.9	33.7	370	5.86	did not peel
A62	1.51	65.4	1.51	150	2.20	did not peel
A63	14.3	36.7	36.7	930	8.50	did not peel
A64	2.37	76.1	2.37	100	1.07	did not peel
A65	9.22	33.8	49.9	910	12.2	did not peel
A66	1.66	59.2	1.66	120	1.74	did not peel
A67	11.9	25.4	37.9	740	12.8	17.9
A68	6.96	58.3	6.96	60	4.88	
A69	2.82	24.7	12.7	190	5.36	20.6
A70	16.3	51.6	35.9	370	16.3	did not peel
A71	7.142	25.2	48.3	750	18.7	588
A72	3.92	38.9	6.61	590	5.15	5.54
						• .

Table 5 - Mechanical Properties

	Stress @ 50% Strain 2 Kg/cm	% Set at 50% Elong– gation	Ultimate Tensile Strength Kg/cm ²	Total Elongation %	Tear Strength	90 [°] Peel Strength
A74	5.42	40.9	11.5	760	5.7	less than
A75	0.517	Too small to measure	5.48	250	0.982	1.8 3.12
A76	44.9	34.8	78.7	250	36.2	380
A77	25.6	31.4	31.1	460	22.8	2.32
A78	25.9	29.0	29.7	50	15.9	163
A79	8.85	34.3	7.38	less than 140	10.9	87.8
A80	11.0	25.0	19.4	390	16.9	205
A81	10.3	41.2	20.6	780	13.5	330
A82	12.5	48.5	13.7	790	11.6	107.7
A83	5.9	26.7	42.0	850	7.6	370
A84	4.32	24.2	32.0	860	6.06	107
A85	1.77	44.5	2.45	1400	1.95	101.2
A86	5.41	26.8	19.5	660	11.8	163
A87	18.3	31.3	19.4	200	17.7	did not peel
A88	12.5	32	13.3	790	8.0	31.0
A89	6.81	35	5.53	270	4.83	33.9
A90	26.6	78	26.8	210	23.6	41.0
A91	32.5	83	32.5	340	25.6	38.7
A92	1.48	39	1.74	1000+	2.18	31.6
A93	1.93	49	2.24	1000+	2.60	64.9
A94	1.91	44	2.10	1000+	2.24	108
A95	1.93	52	2.07	1000+	2.46	105

Table 5 - Mechanical Properties

	Stress @ 50% Strain 2 kg/cm	% Set at 50% Elong– gation	Ultimate Tensile Strength kg/cm ²	Total Elongation %	Tear Strength	90° Peel Strength
	3,					
A96	1.21	66	4.16	230	1.30	1.7
A97	0.579	45	2.8	180 ુ	0.804	2.0
A99	0.701	41	1.32	170	0.953	9.8
A100	2.83	64	7.57	240	3.30	2.7
A101	2.58	86	25.8	120	13.3	17.7
A102	0.482	Too small to measure	0.804	260	0.601	17.4
A103	0.302	Too small to measure	0.501	260	0.518	11.2
A104	0.914	65	1.02	870	1.12	46.5
A105	0.930	58	1.05	770	1.29	23.9
A106	0.560	76	0.659	520	0.577	12.7
A107	0.649	81	0.649	250	0.482	35.2
A108	15.1		15.1	50	2.55	18.6
A109	25.9	· ·	25.9	50	3.29	8.8
A110	26.4	71	26.4	360	20.0	64.3
A117	1.28	56.8	1.54	1000+	1.89	57.2
A118	1.27	53.6	1.35	1000+	1.85	43.5
A130	1.35	53.0	1.61	860+	1.66	47.4
Parafilm	27.7	87	27.7	300	22.3	

Table 6 - Performance of Leak Detection Systems

Coating	Release	Adhesive	# Bubbles/# Leaks	Lift Distance mm	Comments
A48	B2		8/9	2-4	Brush application
A51	B2		1/7	2	11 11
A55		C4	4/5.	₂ -3·	n u
A55		C6	3/5	2	II II
A56	B2	-	4/10	2-3	n n
A57		C 3	5/5	1-3	11 11
A57		C6	5/5	2-4	11 11
A58		C3	5/5	1-3	n u
A 58		C6	4/5	3-4	u u
A59		C 7	0/2	· '	11 11
A59	· · · · · · · · · · · · · · · · · · ·	C3	0/1		ty sı
A75	В3		6/9	3-13	
A81	В3		1/3	2	u u
A82	В7	,	1/4	1	11 11
A83	В1		4/8	3-6	t1 11
A84	В8		4/8	2-6	11 11
A85 .	В2	van een mei	0/4		Aerosol
A85			0/5		11
A85	В3		2/2	2-3	Brush application
A85	В3		0/3	:	u . u
A90	В6		0/1		n n
A90	B1		0/1		. и и
A90	В9		2/2	2	и .
A90			0/0		$\mathbf{u} = \mathbf{v} + \mathbf{u}$
	•		•		

Table 6 - Performance (Cont.)

Coating	Release	Adhesive	# Bubbles/# Leaks	Lift Distance mm	Comments	
A91	В9		1/3	3	Brush applicatio	on
A91	B2 B		1/1	2	tt II	
A91	Bl		2/2	. 1· · ·	n n	
A91	В6		0/1		п	
A91			0/2		11	
A92	B2B		0/4	m = ==	, ii ii	
A92	B1		2/4	10-13	. п п	
A92	В9		5/5	1-3	н н	
A93	B2B		1/4	2	я и	
A93	B1		1/4	10	u u	
A94	B2B		0/3		n ii	
A94	В1		1/1	25	' H II	
A94	В3		0/0		ii ii	
A94	В8		4/4	2-3	. 11	
A94	В9		0/0		11 11	
A94	В9		3/4	2-8	11 11	
A95	В3		0/0		U H	
Á95	В8		0/0		H H	•
A95	В9		0/0		и	
A96	· ,	C3	0/9		0 - 11	
A97	'	C3	0/0	time take said	н п	
A97	B11		6/6	3-13	. 11 11	
A97	B6		0/0		11 11	,
A99		C3	3/3	2-3	H H	

Table 6 - Performance (Cont.)

Coating	Release	Adhesive	# Bubbles/# Leaks	Lift Distance mm	Comments
A100	B2B		2/2	2	Brush application
A100	B1		2/2	, J	11 11
A100	В9		2/2	2	
A100			2/3	3	u u
A101		C3	1/1	2	11
A101	B12		6/6	3-5	: 11
A101	B7 .		1/1	2	11 11
A102	В7		0/1		11 11
A102			1/1	1	и
A102	B2 B		2/2	1	и и
A102	B1		0/2		18 11
A102	В9		1/2	2	n u
A103	B7	·	0/2		n n ·
A103			0/1		u . a
A103	B2B		0/2		и . и
A103	ВТ		1/2	1 .	11
A103	В9		0/3		11 11
A104	В7		0/1		н н
A104			0/1		11 11
A104	B2B		0/1		и и
A104	B1		0/1	have find often	. 0 0
A104	В9		3/3	1	11 11
A105	В9		3/3	3-35	II u
			•		

Table 6 - Performance (Cont.)

Coating	Release	Adhesive	# Bubbles/# Leaks	Lift Distance mm	Comments
	\$ 1 m				
A105			0/1		Brush application
A105	B7		0/1	:	н н
A105	B2B	*	1/1	~ 2	n i
A105	B1 -		2/2	2	11 11
A105	В9		5/5	3-10	n , n
A105	B13	·	0/7		att a
A105	B14		2/6	3	, II II
A105	B15		0/3	iga qua min	11
A105	B10	w = =	9/9	3-25	11 11
A105	B10		9/10	3-6	11 11
A106	В9		3/3	2-13	и и,
A106			0/1 .		H H
A106	B7		0/1		н
A106	B2B		2/2	1-2	11 11
A106	B1		1/1	2	ti ii
A107	В9		0/1		11 11
A107			0/1		11 11
A107	В7		0/1		n n
A107	B2 B	-	0/2		н
A107	B1 - 37		2/2	2	n n
A110	B2 B		3/3	1	п
A110	B1		1/2	. 1	n u
A110	B7		0/2		н ′ н
A110	В9		3/3	3-8	п

Table 6 - Performance (Cont.)

Coating	Release	Adhesive	# Bubbles/# Leaks	Lift Distance	Comments
				mm	:
	-0		- 10		
A110	В9		7/9	2-5	Brush application
A112	В9		10/10	2	11 11
A114	В3	-	0/2		H , H
A114			0/1		H H
A114	B1		0/0	. ===	$\mathbf{u} \rightarrow \mathbf{u}$
A114	В9		0/2		n n
A115	В3		0/3		n n
A115	-	· 	0/0		H H
A115	: B1		2/2	13-35	H H
A115	В9		0/1	••	11 14
A117	B10		3/5	2	11 11
A118	B10		6/6	2-5	11 11
A119	B10		5/7	1-13	II II
A130	B10	allie will pass	9/9	4-25	n n
A130	B10		9/9	3-35	н
A130	B10		10/10	5-20	и и
A130	B10		7/7	3-25	n a ·
A131	B1		0/1	-	Aerosol
A131			0/1		n ·
A131	В3		0/1		u
A131	B10		0/1	-	n ·
A134	B10		7/9	3-25	u
A130	B10		8/8	3-25	Brush application
A130	B10		8/9	5-38	11 15

Table 6 - Performance (Cont.)

Coating	Release	Adhesive	# Bubbles/# Leaks	Lift Distance	Comments
	,			mm	
A130	B10		9/9	3-51	Brush application
A130	B10		9/9	3-19	и и
A130	B10		10/10	3-51	H · ·
A130	B10		5/5	5-10	u u
A130	B10		6/6	5-19	u 8
A130	B10		5/6	5-12	11
A130	B10		10/10	3 -2 5	n n
		·			÷
Total perf	ormance tes	ts with recom	mended system:		

105/107

A130

B10

Brush application

3-51

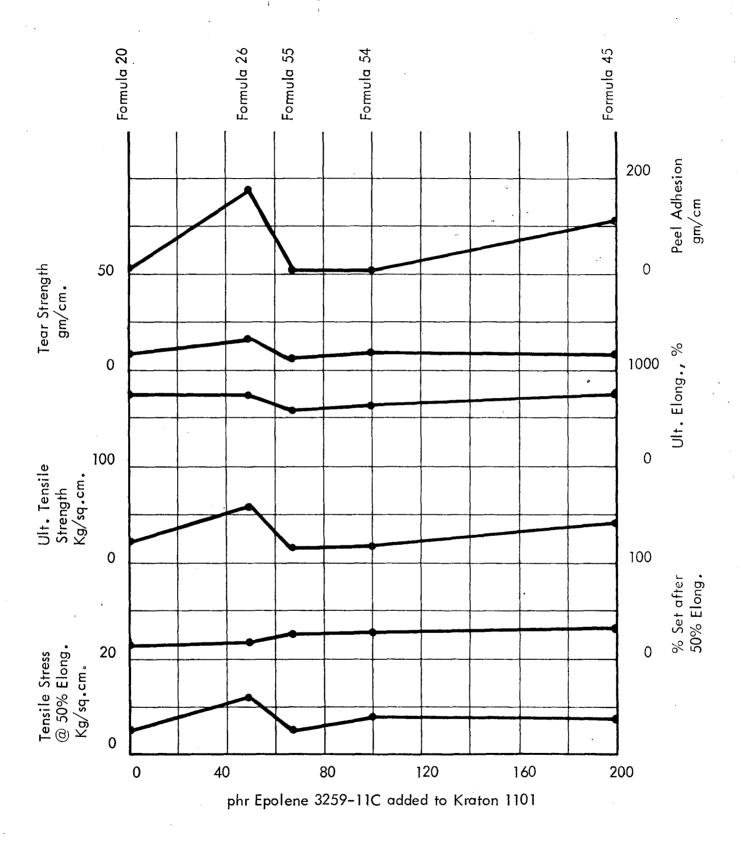


Figure 1 - Effects of Polypropylene Wax Added to Kraton Rubber Formulas

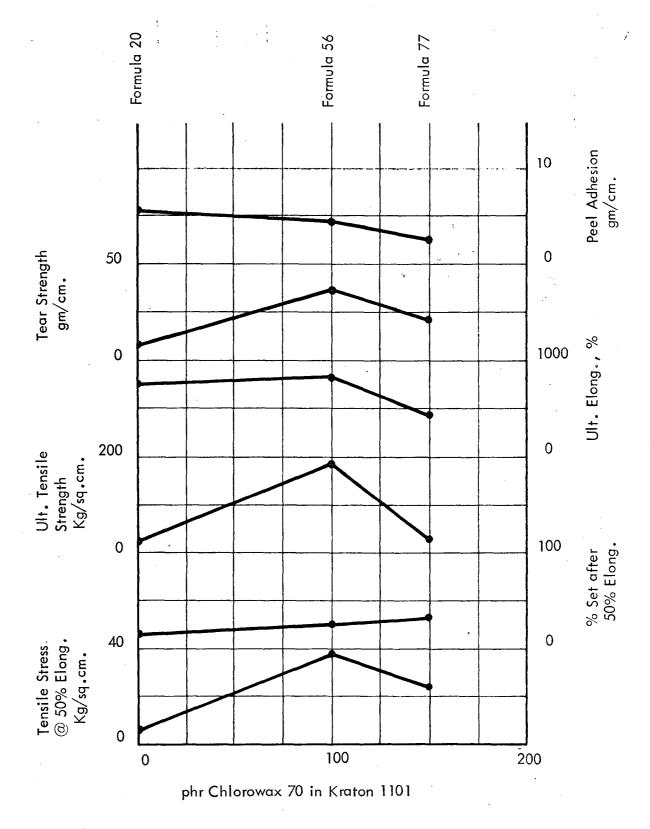


Figure 2 - Effects of Chlorowax 70 Added to Kraton 1101 Rubber

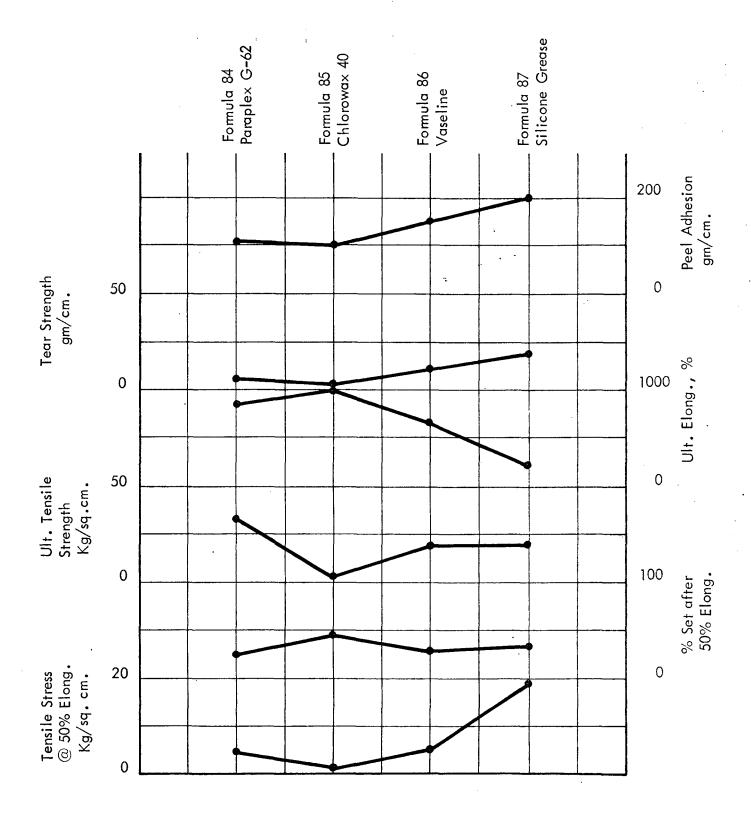


Figure 3 - Effects of Four Plasticizers Added to Kraton 1101 Rubber with Chlorowax 70

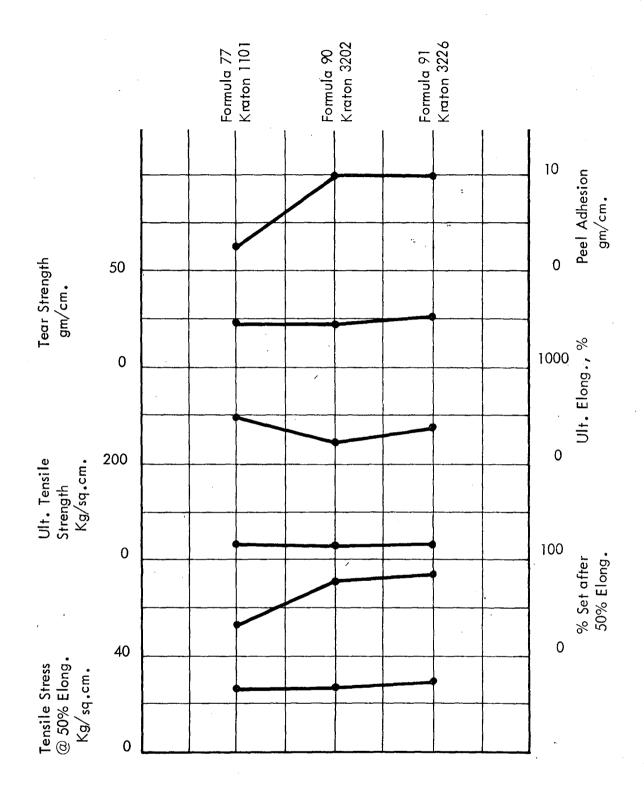


Figure 4 - Comparison of Three Different Kraton Rubbers used with 150 phr Chlorowax 70.

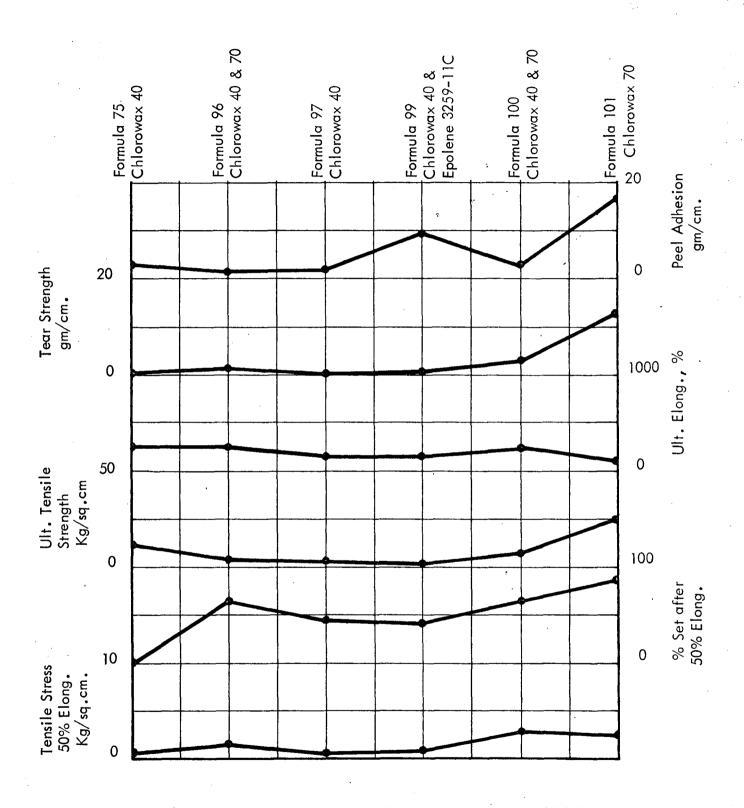
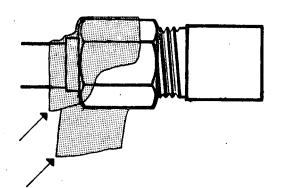
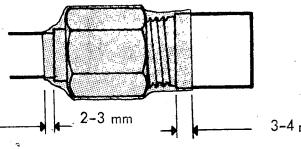


Figure 5 - Effects of Plasticizers and Waxes Added to Vinyl Resin VYHH and Paraplex G-62



Figure 6 - Performance Evaluation of Leak Detection Systems under Water. Expanded coatings are readily discernible on two connectors.



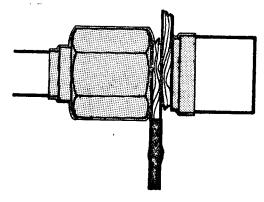


Stretched tightly to conform, then wrapped tightly.

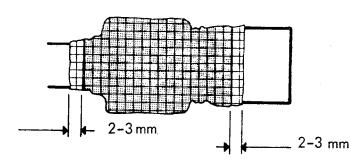
3-mil Parafilm

A. Parafilm Tape Application.

B. Helical wrap of Parafilm for complete coverage beyond connector and threads.



C. Parafilm pulled tightly at both ends of connector with bundle of elastic threads.



D. Two coats of expandable coating applied over the Parafilm and onto tubing to seal the connector.

Figure 7 - Step-wise Application of Parafilm Release Tape and Expandable Coating for Leak Detection System.